



Color and Nitrogen Removal from Synthetic Dye Wastewater in an Integrated Hydrolysis/Acidification and Anoxic/Aerobic Process

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2018.10.15



Content

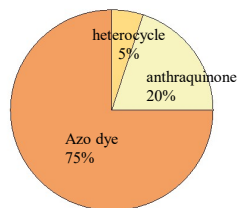
1. Background
2. Materials and Method
3. Results and Discussion
4. Conclusion

1. Background



1.1 Dyeing industry and dyeing wastewater

■ Production and characteristic of dyeing wastewater



Distribution of dye (Zhao et al., 2018)

| Cotton | Wool | Silk | Dacron | Polyester cotton |
|----------|------|--------|----------|------------------|
| Direct | Acid | Acid | Disperse | Disperse |
| Active | | | | |
| Reducing | | Direct | Azo | Reducing |
| Azo | | | | |

Dye used in different industries

Dyeing wastewater

17-20% industry wastewater



COD



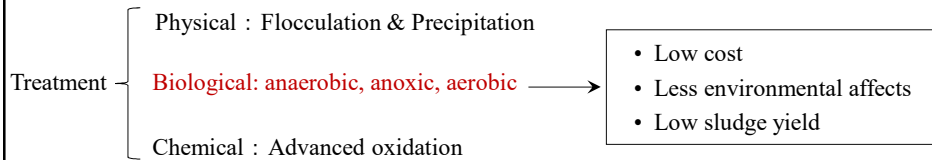
Color



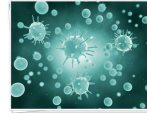
NH₄-N

1.2 Technology for color removal

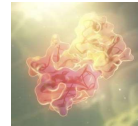
■ Treatment of dyeing wastewater



(Chandrakant et al., 2016; Wang et al., 2011)



- Dye degradation is based on the function of microorganisms
- Anoxic/aerobic is the most common process for dye degradation
- The color removal efficiency depends on the structure of microbes and the activity of enzymes

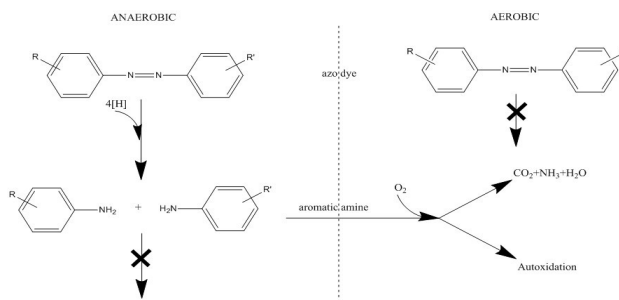


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1.2 Technology for color removal

■ Biodegradation mechanism for azo dye

- Breaking the azo bond $-N=N-$
- Aromatic amine compounds generated with 4 electrons for breaking the azo bond in anaerobic process
- The intermediates can be removed by complete mineralization or autoxidation



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1.2 Technology for color removal

■ Biological treatment of azo dye

- Biological treatment for azo dye usually needs long HRT, high COD
- Color removal efficiency can not reach 100%

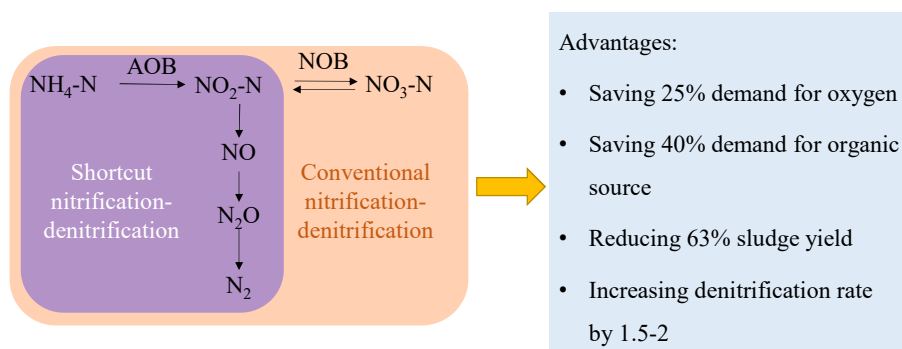
| Reactor type | dye | Temperature (°C) | HRT (h) | COD (mg/L) | Color removal(%) | Reference |
|--------------|-------|------------------|---------|------------|------------------|------------------------|
| SBR | DR80 | 35 | 48 | 500-3000 | 69.1-98.23 | Kashif et al., 2015 |
| ABR+FAS | RR2 | 35 | 24 | 4000 | 89.5 | Naimabadi et al., 2009 |
| SBR | AR14 | / | 6 | 1000 | 85 | Franca et al., 2015 |
| SBR | Mixed | 27 | 24 | 1017 | 70-80 | Tomei et al., 2016 |
| PBB | VBR | / | 48 | 300 | 99.2 | Chen et al., 2016 |

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1.3 Enhanced nitrogen removal for dyeing wastewater

■ Biological nitrogen removal

Advantages of shortcut nitrification-denitrification for wastewater



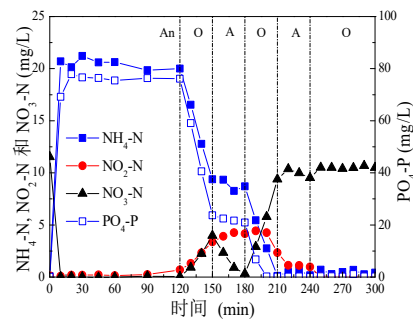
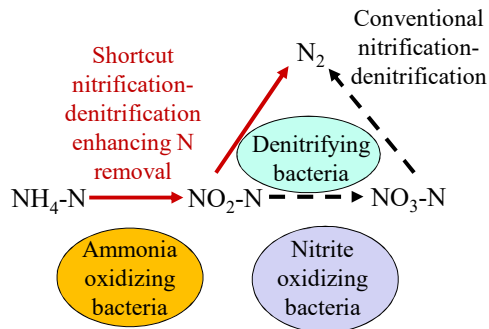
(Abeling and Seyfried, 1992; Bernet et al., 2001; Fux et al., 2006; Wang and Yang, 2004)

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1.3 Enhanced nitrogen removal for dyeing wastewater

■ Enhanced nitrogen removal by multiple AO process

To solve the lack of COD in influent of wastewater, the inhibition of NOB could enhance nitrogen removal through shortcut nitrification-denitrification with multiple AO process



Multiple AO operation mode could control microbial ecology and enhance nitrogen removal

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1.4 Requirements and purposes for research

■ Technical requirements of biological treatment

- **Color removal :**

The lack of researches on the azo dye degradation pathway and the functional microbial community in biological treatment

- **Nitrogen removal :**

The lack of researches on the nitrogen removal and the application of shortcut nitrification-denitrification in dyeing wastewater treatment

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1.4 Requirements and purposes for research

■ Purposes

- The system performance of hydrolysis/acidification and anoxic-aerobic(AO) treatment for azo dye wastewater
- The factors influencing color removal efficiency and the pathway of azo dye in hydrolysis/acidification process
- The factors influencing nitrogen removal in AO process
- The microbial community in the hydrolysis/acidification and AO process

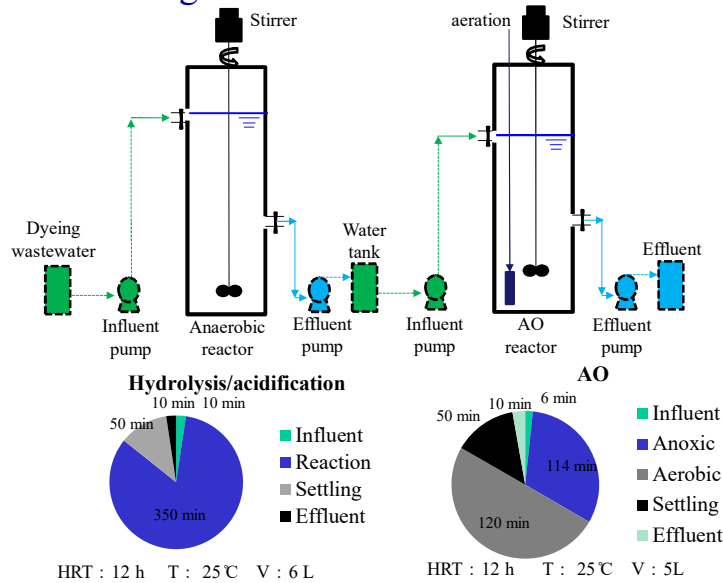
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2. Materials and Methods



2.1 Experimental setup

■ Schematic diagram



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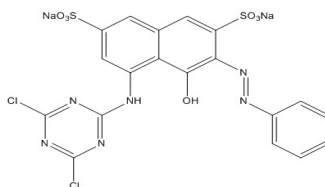
2.1 Experimental setup

■ Components

| Components | Concentration (mg/L) | Components | Concentration (mg/L) |
|--------------------------------------|----------------------|--------------------|----------------------|
| NH ₄ Cl | 114.6 | NaHCO ₃ | 200 |
| Azo dye (RR2) | 30 | Sodium Acetate | 51.28 |
| KH ₂ PO ₄ | 35.2 | Starch | 224.93 |
| MgSO ₄ ·7H ₂ O | 100 | Peptone | 109.09 |
| CaCl ₂ ·2H ₂ O | 100 | Trace elements | 1 mL/L |

Mixed carbon source= 1:3:6 COD=400 mg/L

Azo dye
Reactive Red 2



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2.2 Method

■ Methods

- COD, NH₄-N, NO₂-N, NO₃-N, MLSS, MLVSS: APHA
- Color: the absorption of azo dye RR2 in 512 nm

$$\text{Color removal efficiency (\%)} = \frac{A_0 - A}{A_0} \times 100$$

A₀: absorption of influent A: absorption of effluent
- QTOF detection : Combined Q-TOF MS (Agilent 6560 IM Q-TOF) and LC system (Agilent 1290 Infinity, USA) (LC-IM-QTOF-MS)
- Aniline : LC-MSMS, combined LC system (LC-20AD, Shimadzu, Japan) and mass spectrometer (API 3200, AB Sciex, U.S.)
- Microbial community: 16s rRNA

Condition in mass spectrometer

| | |
|------------------|--------|
| Curtain Gas | 10 psi |
| Collision Gas | 6 |
| IonSpray Voltage | 5000 V |
| Temperature | 400 °C |
| Ion Source Gas 1 | 60 psi |
| Ion Source Gas 2 | 60 psi |

MRM condition for aniline

| | Q1/Q3 | DP | EP | CEP | CE | CXP |
|-------------------------------|-----------|------|------|------|------|-----|
| Quantitative Q1/Q3 transition | 94.2/77.1 | 21.0 | 11.5 | 12.0 | 27.0 | 4.0 |
| Qualitative Q1/Q3 transition | 94.2/51.1 | 21.0 | 11.5 | 12.0 | 45.0 | 4.0 |

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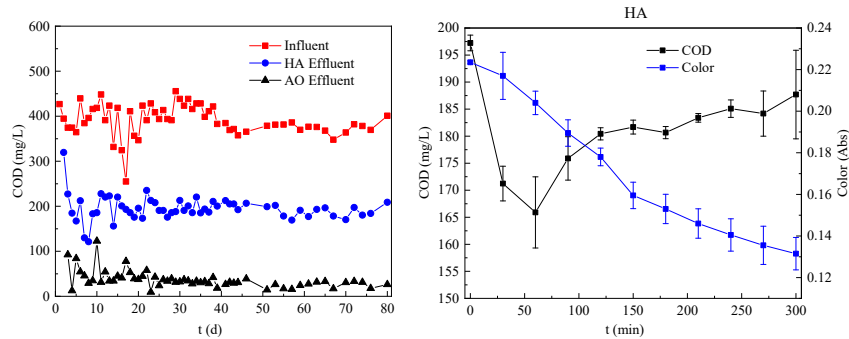
3. Results and Discussion



3.1 System performance

■ COD

- Concentration of COD did not change much in the hydrolysis/acidification process
- COD was removed in the denitrification process



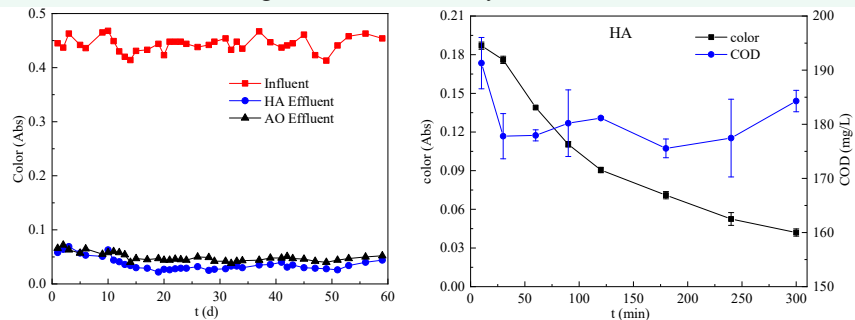
| | Influent (mg/L) | HA effluent (mg/L) | AO Effluent (mg/L) | Removal efficiency (%) |
|------------|--------------------|-----------------------|-----------------------|---------------------------|
| COD | 381.5±27.7 | 178.1±24.6 | 19.5±9.0 | 94.9 |

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3.1 System performance

■ Color

- Hydrolysis/acidification was the main process for color removal
- AO effluent had higher color
- Some intermediates generated from azo dye could have a reverse reaction

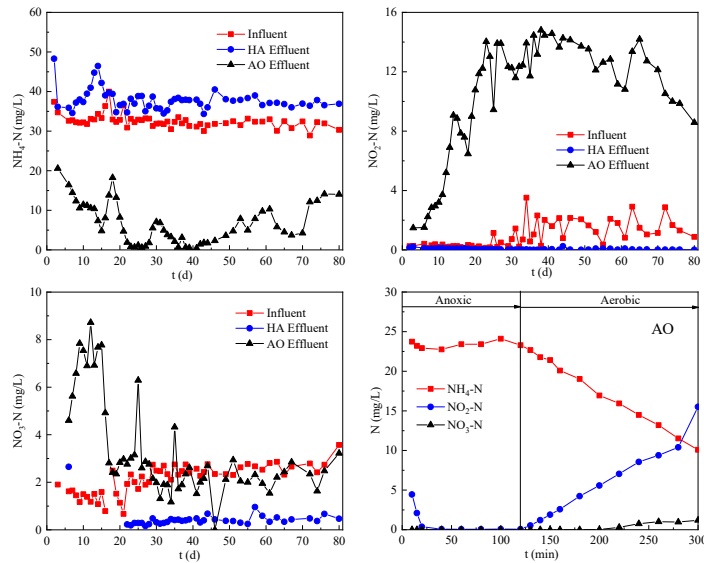


| | Influent | HA effluent | AO Effluent | Removal efficiency (%) |
|--------------|--------------------|--------------------|--------------------|---------------------------|
| Color | 0.442±0.014 | 0.033±0.008 | 0.047±0.005 | 89.4 |

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3.1 System performance

■ Nitrogen



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3.1 System performance

■ Nitrogen

| | Influent (mg/L) | HA effluent (mg/L) | AO Effluent (mg/L) | Removal efficiency (%) |
|------------------------|------------------|--------------------|--------------------|------------------------|
| $\text{NH}_4\text{-N}$ | 31.74 ± 1.11 | 37.42 ± 1.39 | 5.23 ± 4.29 | 83.5 |
| $\text{NO}_2\text{-N}$ | 1.54 ± 0.84 | 0.03 ± 0.04 | 11.03 ± 3.96 | / |
| $\text{NO}_3\text{-N}$ | 2.72 ± 0.49 | 0.48 ± 0.19 | 4.39 ± 5.72 | / |

- Nitrite accumulation
- Removal efficiency of total inorganic nitrogen (TIN) : 42.6%

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3.2 Color removal during hydrolysis/acidification

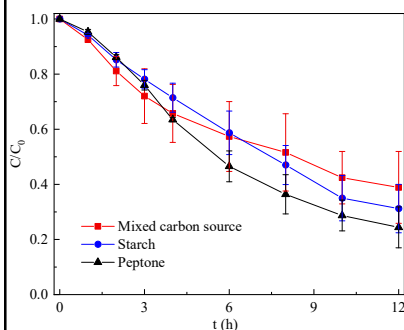
■ Effects of carbon source and temperature on color removal

- Seed sludge: sludge from hydrolysis/acidification reactor under steady condition
- Reaction volume: 500 mL
- Mixing speed: 170 rpm
- Temperature: 25 °C and 35 °C
- Influent components: same as the reactor; carbon source (COD= 400 mg/L, Peptone, Starch and mixed carbon source); COD concentration (COD=200, 400, 800 mg/L, mixed carbon source=1:3:6)

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3.2 Color removal during hydrolysis/acidification

■ Effects of carbon source



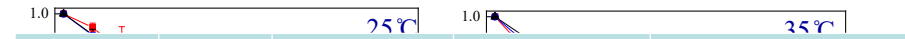
| Carbon source (COD=400 mg/L) | First order kinetics equation | Degradation rate(mg/(L·h)) | COD removal efficiency (%) |
|------------------------------|-------------------------------|----------------------------|----------------------------|
| Mixed carbon source | $y=e^{-0.085x}$ | 2.55 | 59.99 |
| Peptone | $y=e^{-0.097x}$ | 2.91 | 63.64 |
| Starch | $y=e^{-0.121x}$ | 3.63 | 44.01 |

- Degradation of RR2 was non-specific
- Degradation of RR2 fitted the first order kinetics equation
- When starch was used as carbon source, degradation rate was the fastest, followed by peptone and mixed carbon source

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3.2 Color removal during hydrolysis/acidification

■ Effects of COD concentration and temperature



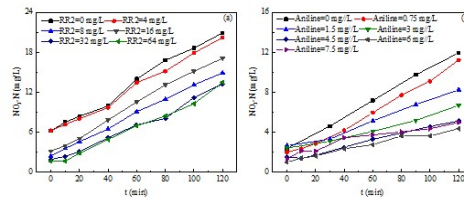
| Temperature | COD (mg/L) | First order kinetics equation | Degradation rate (mg/(L·h)) | COD removal efficiency (%) |
|-------------|------------|-------------------------------|-----------------------------|----------------------------|
| 25 °C | 800 | $y=e^{-0.139x}$ | 4.17 | 57.46 |
| | 400 | $y=e^{-0.085x}$ | 2.55 | 59.99 |
| | 200 | $y=e^{-0.045x}$ | 1.35 | 57.86 |
| 35 °C | 800 | $y=e^{-0.245x}$ | 7.35 | 45.05 |
| | 400 | $y=e^{-0.205x}$ | 6.15 | 54.02 |
| | 200 | $y=e^{-0.149x}$ | 4.47 | 26.31 |

- Degradation rate increased with increasing COD concentrations
- Degradation rate increased apparently with increasing temperature
- Temperature was the main factor affecting the azo dye degradation

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3.3 Nitrogen removal during AO

■ Effects of RR2 and aniline on nitrification



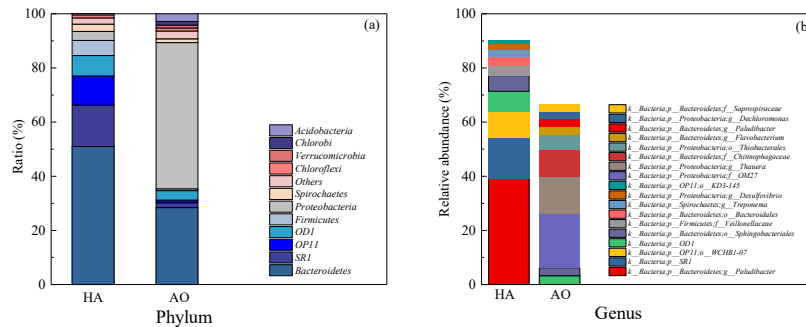
| Aniline (mg/L) | NH ₄ -N | R _{NH4-N} (mg/(gVSS·h)) | NO ₃ -N | R _{NO3-N} (mg/(gVSS·h)) |
|----------------|------------------------|----------------------------------|----------------------|----------------------------------|
| 0 | $y = -0.0763x + 27.41$ | 1.38 | $y = 0.0784x + 3.41$ | 1.42 |
| 0.75 | $y = -0.0852x + 27.03$ | 1.31 | $y = 0.0978x + 1.88$ | 1.51 |
| 1.5 | $y = -0.0541x + 28.19$ | 0.98 | $y = 0.0542x + 2.66$ | 0.98 |
| 3 | $y = -0.0507x + 28.66$ | 0.92 | $y = 0.0415x + 2.37$ | 0.75 |
| 4.5 | $y = -0.0478x + 27.24$ | 0.74 | $y = 0.0415x + 1.54$ | 0.64 |
| 6 | $y = -0.0345x + 26.71$ | 0.53 | $y = 0.0345x + 1.39$ | 0.53 |
| 7.5 | $y = -0.0371x + 28.65$ | 0.57 | $y = 0.0356x + 2.18$ | 0.55 |

- RR2 had no obvious effects on nitrification process
- Aniline could inhibit nitrification process
- When aniline reached 6 mg/L, nitrification was inhibited

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3.4 Microbial community

Hydrolysis/acidification and AO

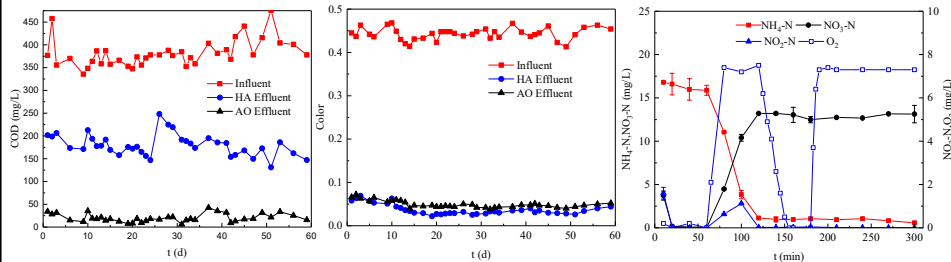


- The dominant bacteria in hydrolysis/acidification: *Paludibacter*, *SRI*, *OP11* and *OD1*
- *Desulfovibrio* (relative abundance: 2.23%) was mainly responsible for azo dye degradation (Xie et al., 2018)
- The dominant bacteria in AO: *Myxococcales*, *Thauera*, *Chitinophagaceae*, *Thiobacteriales*, *OD1* and *Flavobacterium*
- *Thauera* was a typical shortcut denitrifying bacteria (Fernandes et al., 2018)

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3.5 Hydrolysis/acidification-multiple AO process

System performance

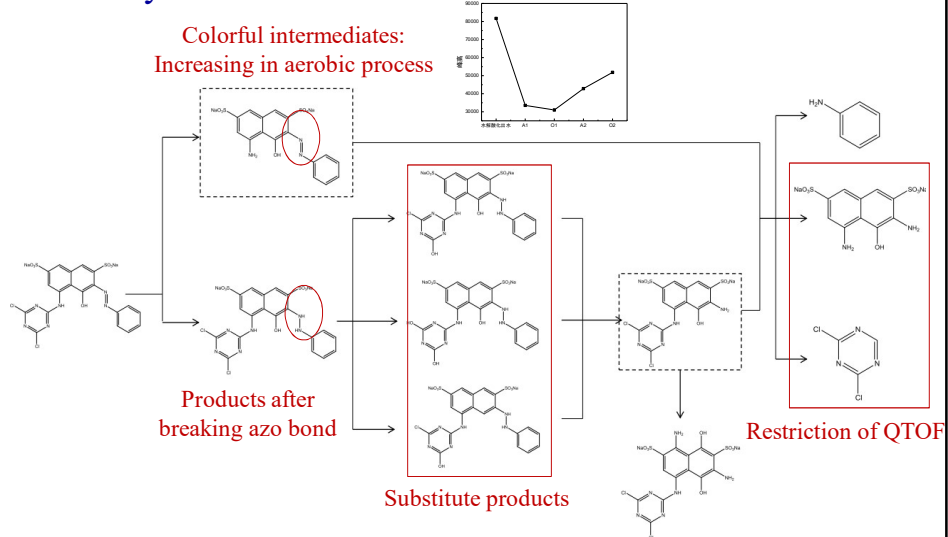


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| COD | 381.5±27.7 | 178.1±24.6 | 19.5±9.0 | 94.9 |
| Color | 0.442±0.014 | 0.033±0.008 | 0.047±0.005 | 89.4 |
| NH ₄ -N | 22.53±1.87 | 29.23±2.58 | 0.53±0.18 | 97.64 |
| NO ₂ -N | 1.79±0.94 | 0.01±0.00 | 0.02±0.01 | 98.89 |
| NO ₃ -N | 3.47±1.20 | 0.56±0.18 | 13.75±1.14 | / |

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3.5 Hydrolysis/acidification-multiple AO process

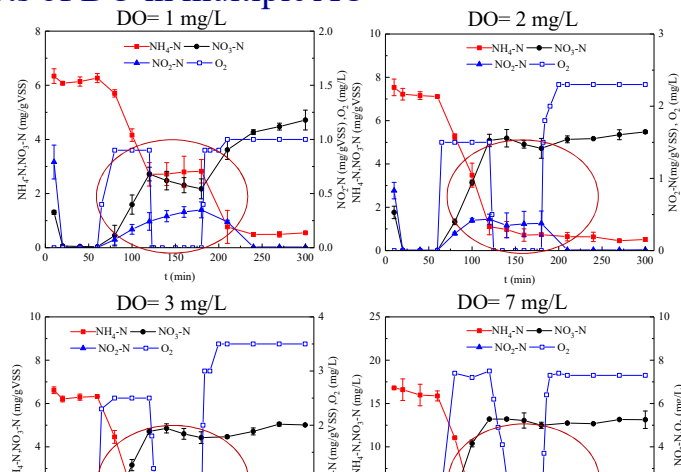
■ Pathway of RR2 metabolism



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3.5 Hydrolysis/acidification-multiple AO process

■ Effects of DO in multiple AO

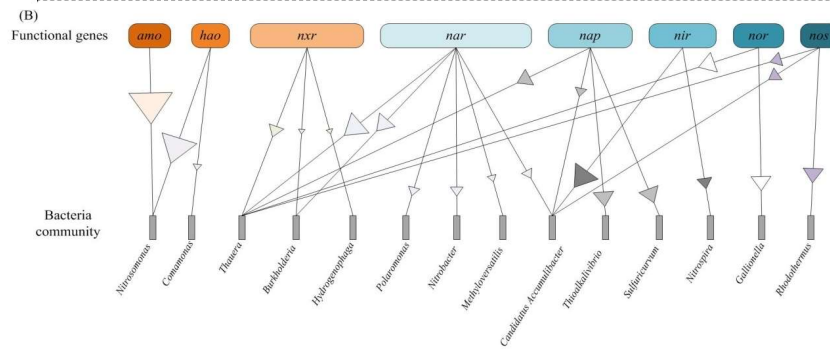


- Low DO could increase TIN removal efficiency
- Low DO could accumulate nitrite, inhibit activity of NOB

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3.5 Hydrolysis/acidification-multiple AO process

■ Functional genes in nitrogen metabolism



- Nitrification: *Nitrosomonas*, *Nitrospira*, *Comamonas*, *Thauera*
- Denitrification: *Thauera*, *Candidatus Accumulibacter*

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4. Conclusion



4. Conclusion

- Hydrolysis/acidification-AO and hydrolysis/acidification-multiple AO process could treat dyeing wastewater efficiently
- The main factors affecting color removal were carbon source, COD concentration and temperature
- The main factors affecting nitrogen removal were azo dye, intermediates and DO
- The dominant bacteria for azo dye degradation were *Desulfovibrio aminophilus*, *Thermoanaerobacter*, *Lactococcus raffinolactis*, *Ruminiclostridium* and *Rhodopirellula*

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Thank you for your kind attention!

